EXPERIENCES IN MONITORING AIRBORNE RADIOACTIVE CONTAMI-NATION IN JAERI

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In Japan Atomic Energy Research Institute(JAERI) there are many facilities and laboratories where the protection from airborne radioactive materials is more important than that from external radiation. In them air monitoring is indispensable to confirm the kinds and amounts of airborne radionuclides and estimate the personnel exposure dose due to these atmospheric contaminants.

This report describes some problems which have been experienced in air monitoring for hot cells for handling highly radioactive materials, glove boxes for handling plutonium and a cell for producing 99Mo.

DISPERSION FACTOR

When irradiated uranium metal fuel was cut in a hot cell, the ratio of activity of airborne dust to that of the whole dust was determined for representative nuclide (1). The dispersion factor $\epsilon(k)$ for nuclide k was defined as

$$\varepsilon(k) = D(k) / M(k)$$

D(k) is the activity of nuclide k dispersed in the air in a hot cell when the fuel was cut; it was evaluated from the concentration of airborne nuclide k activity, the volume of the hot cell(144m³) and the ventilation rate of the cell(10 volumes/h). M(k) is the total activity of nuclide k contained in the cut dust; it was calculated from the irradiation history of the fuel. Airborne radioactive dust in the hot cell was collected on a cellulose-asbestos filter paper(Toyo HE-40) and a charcoal- loaded filter paper(Toyo CP-20). The activities of the dust were determined using a gamma-spectrum analyzer with a 5"x4"NaI(T1) scintillation detector.

The results showed that the dispersion factors were the order of 10^{-2} for semi-volatile form of $^{1\,2\,5}Sb$ and $10^{-3}\,\sim\,10^{-4}$ for particulate forms of $^{1\,3\,7}Cs$ and $^{1\,4\,4}Ce^{-^{1\,4\,4}}Pr.$

SIZE DISTRIBUTION OF RADIOACTIVE AEROSOL

For radioactive aerosols produced during works (mainly decontamination in the hot cells), the size distributions were investigated with a 4-stage cascade centripeter developed by U.K.A.E.A..

Radioactive aerosols were collected by the centripeter operated at flow rate 20 l/min for the work duration(10 min \sim 2 h). The representative size(expressed as aerodynamic diameter) for each stage of the instrument at flow

Table 1 Size distributions of radioactive aerosols produced during various works at the hot laboratory

| Group | Radiation work | Height of sampling point (m) | Size distribution | |
|-------|---|------------------------------|-------------------|-----------------------|
| | | | AMAD (µm) | σg |
| | Decontamination of the hot cells | 0.7-1.1 | 2.5-11 | 1.7-3.2 (1.6-1.9)* |
| | Exchange of the exhaust filters | 0.3 1.1 | 7.0 | 1.7 |
| | Overhauling in the hot cells(1) | 1.1 | 6.5 8.0 | 1.8 2.0 |
| A | Handling of the contaminated container | 0.3 0.7 | 8.5 12 | 1.8 |
| | Handling of irradiated graphite | 0.6 | 15 | 2.8 |
| | Dismantling of the hot drain pipe | 1.1 | 9.0 | 1.7 |
| В | Overhauling in the hot cells (include weld- ing) (2) | 0.3 | 0.41 | 7.1 12.5 |

^{*} Size results of aerosol with alpha activity.

rate 20 1/min was calculated from the data(the effective cut-off sizes for the four stages at flow rate 30 1/min) given by Hounam, R.F. and Sherwood, R.J.(2) and O'Connor, D.T. (3), using the relationship that the aerodynamic diameter of aerosol is inversely proportional to the square root of the flow rate on the basis of impaction theory. Activity median aerodynamic diameter (AMAD) and geometric standard

deviation(σ_g) of the size distribution were estimated graphically on a log-normal probability paper, assuming a linear relationship between cumulative percentage of the activity on each stage and the representative size.

In Table 1 are shown aerosol size results for 24 aerosol samples with beta activity and for 3 samples with alpha activity. AS seen in Table 1, the AMAD and σ_g of the size distributions in usual radiation works(group A) are in the range of 2.5 \sim 15µm and 1.6 \sim 3.2, respectively. The most remarkable in the present investigation was group B having AMAD less than lµm with σ_g of larger than 7. Such fine, respirable aerosols could be produced by high temperature burning in the air of radioactive contaminants within the cell due to arc welding.

RESUSPENSION FACTOR

In a plutonium handling laboratory, surface materials of the floor and equipments were contaminated extensively by particulate plutonium oxide(PuO2) due to break of the negative pressure in a glove box. Therefore, the suspension factor(the ratio of the concentration of airborne contamination to the level of surface contamination) had to be evaluated to determine the procedure of decontamination and the type of respiratory equipment. Two workers who wore Harwell self-contained air-ventilated blouses, moved around in a PVC sheeting tent to fix the contaminant and seal up the leakage positions on the glove box. Volume and area of the contaminated floor inside the tent were about 6 $\rm m^3$ and 2 $\rm m^2$, respectively, and its ventilation rate was 10 volumes/h. Floor surface was almost uniformly contaminated at 4.5 x $10^{-2}~\mu\text{Ci/cm}^2$. The contamination was measured with a ZnS scintillation survey meter. Airborne contaminant was sampled with a personal air sampler, and its particle sizes were evaluated by autoradiographic technique. The particle size distribution was in the range of mass median diameter (MMD) 6.4 to 26µm, and og was from 2.3 to 2.7.

The resuspension factor was found to be $4 \times 10^{-8} \sim 2 \times 10^{-7} \text{cm}^{-1}$ for plutonium oxide particles deposited on the floor surface. The values agreed well with those obtained by Jones, I.S. and Pond, S.F. (4).

COLLECTION EFFICIENCY OF CHARCOAL-LOADED FILTER PAPER FOR AIRBORNE RADIOIODINE

A new charcoal-loaded filter paper (Toyo CP-20T) was made in order to improve collection efficiency of CP-20 filter papers and decrease its air resistance. Specifications of CP-20 and CP-20T filter papers are shown in Table 2. The radioiodine generated in 99 Mo production process was used for test, and consisted of 60% inorganic and 40% organic iodide. The chemical forms were determined with a sampler modified Maypack(5). The test conditions of air

flow through filter papers were relative humidity 40 \sim 80 %, face velocity 50 cm/sec and flow time of iodine 4 \sim 18h.

Table 2 Comparison of specifications of charcoal-loaded filter paper

| g | Charcoal-loaded filter paper | | |
|--------------------------------|------------------------------|-----------------|--|
| Specification | CP-20 | CP-20T | |
| Weight (g/m²) | 700 | 650 ∿ 700 | |
| Thickness (mm) | 2.0 | 2.2 | |
| Base material | Cellulose-asbestos fiber | Glass fiber | |
| Activated charcoal | Tsurumi coal HC | Tsurumi coal HC | |
| Size of charcoal granule(mesh) | 60 ∿ 200 | 60 ∿ 200 | |
| Charcoal content(wt | %) 45 | 75 | |

Following are the results:

- (1) Collection efficiencies with and without the triethylenediamine (TEDA) impregnated charcoal were found to be greater than 95 % and about 80 %, respectively.
- (2) Air resistance across the new filter paper decreased to less than $1/2\,(0.8\,\mathrm{mmHg}$ rise/cm face velocity) compared with CP-20.
- (3) Iodine retention efficiency of CP-20T during 24h following start of air flow was greater than 95 %, thereafter, there was found no more desorption of iodine.

REFERENCES

- 1. Izumi, Y., Matsui, T., Ikezawa, Y. and Tanabe, I. (1978): Hoken Butsuri, 13, 295.
- 2. Hounam, R.F. and Sherwood, R.J. (1965): Amer. Hyg. Assoc. J. 26, 122.
- 3. O'Connor, D.T. (1971); AHSB(RP)-108.
- 4. Jones, I.S. and Pond, S.F. (1964): In: Proceedings, Surface Contamination, p.83. Editor: B.R.Fish. Pergamon Press London-New York.
- 5. Keller, J.H., Thomas, T.R., Pence, D.T. and Maeck, W.J. (1971): In: Proceedings, 12th AEC Air Cleaning Conference, p.322. Editor: M.W.First and J.M.Morgan, Jr., CONF-700816.